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NASA

HUNTSVILLE, ALABAMA

Third Quarterly Progress Report January 1 to March 31, 1963 Development of Ni-Cr-Al Alloys for

High Temperature Tubing Applications

April 15, 1963

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\$ 1.10 pl

MICROFILM \$

by

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> CR-50,758 SQT-7595

Development of Ni-Cr-Al Alloys

for

High Temperature Tubing Applications

Abstract

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Tensile test results are presented for as received strip material aged without prior solution anneal and strip material after heliarc welding or brazing with a nickel-silicon-boron material. The welded samples were processed in two groups. One group of samples was aged prior to welding, while the second group was aged after welding.

This report was prepared by New England Materials
Laboratory, Inc., under Contract No. NAS 8-5085,
"Development of Ni-Cr-Al Alloys for High Temperature Tubing Applications" for the George C. Marshall
Space Flight Center of the National Aeronautics and
Space Administration. This work was administered
under the direction of the Propulsion and Vehicle
Engineering Division, Engineering Materials Branch
of the George C. Marshall Space Flight Center with
W. B. McPherson acting as project manager.

## INTRODUCTION

The Ni-Cr-Al alloy systems offer considerable promise for the development of elevated temperature materials with high strength. In the high Cr-high Al compositions, they may find use as bearings and tools and in the lower Cr-Al range as oxidation resistant sheet. During the course of this program, the Ni-Cr-Al alloy systems will be studied to develop an alloy with high strength, good formability and brazing characteristics for high temperature tubing applications.

## RESULTS

Samples of alloy HM32 were heliard welded. One set of samples was solution treated prior to welding and then aged 20 hours at 1400° F. Tensile tests were conducted at room temperature to 1500° F. The results, shown in Table I, are comparable to that obtained with solution treated and aged strip (Second Quarterly Progress Report). A second set of samples was solution treated and aged 20 hours at 1400° F prior to welding and then tensile tested at room temperature to 1500° F. Although the properties in this case, shown in Table II, were lower than when the samples were aged after welding, the results indicate that repair type welds can be made on structures without significant effect on properties.

Of three brazing alloys investigated for compatibility with N1-Cr-Al alloys, only AMS4778, a nickel-silicon-boron material, effectively wet the nickel-chromium-aluminum alloys. Further heat treatment conducted with this braze and HM32, the alloy selected for tubing, did not result in any detrimental effects as examined by metallography or hardness measurements.

Additional samples of alloy HM32 were brazed with AMS4778 for 30 minutes in hydrogen at 1975° F. The brazed samples were then aged 2 hours at 1400° F and tensile tested at room temperature to 1500° F. The results, shown in Table III, indicate lower strength and ductility as compared to solution treated and aged material (Second Quarterly Progress Report). All failures were in the area of the braze and indicated brittleness. The failures are related to the strength of the braze material rather than a weakness of HM32 from interaction with the braze.

On the basis of aging studies conducted with the as received 1/16" strip (Revised First Quarterly Progress Report), samples were prepared for tensile testing of aged as received strip without a prior solution anneal. Alloy HM31 was aged for 2 hours at 1200° F and alloys HM30 and HM32 were aged at 1400° F for 10 hours and 2 hours respectively. The results of the tensile tests conducted at room temperature to

2000° F are shown in Table IV. In general, the alloys had higher tensile strengths and lower ductilities up to 1500° F as compared to the case when the strip material is solution treated prior to aging. Above 1500° F, there was no significant difference in alloy properties when the strip is aged with or without a prior solution anneal.

Alloy HM32 has previously been selected for the preparation of tubing. Additional material has been vacuum melted and processed through preliminary breakdown procedures. Experiments are now in progress towards producing tubing.

## FUTURE WORK

The major effort during the next report period will be devoted toward the preparation of extruded tubing of alloy HM32.

TABLE I. Tensile Properties of Wolded HW32 Strip Aged for 20 Water at 1400° F after Welding

Temperature	U.T.S. (rs1)	0.2% Y S. (psi)	Telil :	48:A:	
Room Temp	143,000	73,400	13	1.7	
900° F	121,000	61,500	12	5	
1200° F	98,500	52,400	8	16	
1500° F	42,700	22,600	26	21	

TABLE II. Tensile Properties of HM32 Strip Welded after Aging for 20 Hours at 1400° F.

Temperature	U.T.S. (psi)	0 2% Y.S. (osi)	%Els	%R A
Room Temp	93600	41,200	71	49
900° F	80.600	40,000	36	62
1200° F	66,500	၁၈ , ၈၀၀	33	5 <u>Z</u>
1500° F	30.360	22 <sub>0</sub> 800	43	31

TABLE III. Tensile Proporties of Brazed HMB2 Strip Aged for 2 Hours at 1400° F after Brazing.

Temperature	U.T.S. (psi)	0.2% Y.S (nsi)	%P1.	%R;A;	
Room Temp	100.000	65,300	G		
300; Ł	70,800	31.200	5	4	
12 <b>0</b> 0° F	80 ,0C0	(i) , i(0)	3	7	
2500° F	33.000	31.000	-	% ≱.	

KABLE 1V

Tensile Test Results

Specimens Machined from 1/16" Stain

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RM308	207,500	271,000	123,600	48,700	001 17	2,200	As macelved strip house at 1400° F
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"\*Specimen broke in bolder